

361(6): The Acceleration in Dynamics as a Cartesian and Lagrange Derivative.

Consider the velocity \underline{v} in plane polar coordinates:

$$\underline{v} = v_r \underline{e}_r + r\dot{\theta} \underline{e}_\theta \quad - (1)$$

$$= \dot{r} \underline{e}_r + v_\theta \underline{e}_\theta$$

$$= v_r \underline{e}_r + v_\theta \underline{e}_\theta$$

From ECE2 theory the acceleration is:

$$\underline{a} = \frac{D\underline{v}}{Dt} = \frac{\partial \underline{v}}{\partial t} + (\underline{v} \cdot \nabla) \underline{v} \quad - (2)$$

Note carefully that this is a general result valid for both dynamics and fluid dynamics. It is the result of ECE2 unified field theory, and is a new result of dynamics.

From previous notes:

$$\frac{D\underline{v}}{Dt} = \frac{\partial v_r}{\partial t} \underline{e}_r + \frac{\partial v_\theta}{\partial t} \underline{e}_\theta$$

$$+ \left(v_r \frac{\partial v_r}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_r}{\partial \theta} - \frac{v_\theta^2}{r} \right) \underline{e}_r \quad - (3)$$

$$+ \left(v_r \frac{\partial v_\theta}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_\theta}{\partial \theta} + \frac{v_\theta v_r}{r} \right) \underline{e}_\theta$$

Now express eq. (3) as a covariant derivative of Cartesian geometry:

$$\underline{a} = \frac{D\underline{v}}{Dt} = \frac{Dv_r}{Dt} \underline{e}_r + \frac{Dv_\theta}{Dt} \underline{e}_\theta \quad - (4)$$

2) Eq. (4) is a new and original definition of any acceleration. -(5)

Therefore:

$$\underline{a} = \frac{d\underline{v}}{dt} + (\underline{v} \cdot \nabla) \underline{v} = \frac{Dv_r}{Dt} \underline{e}_r + \frac{Dv_\theta}{Dt} \underline{e}_\theta$$

The individual covariant derivatives are:

$$\begin{aligned} \frac{Dv_r}{Dt} &= \frac{\partial v_r}{\partial t} + \left(v_r \frac{\partial v_r}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_r}{\partial \theta} - \frac{v_\theta^2}{r} \right) \\ &= \frac{\partial v_r}{\partial t} + \dot{r} \frac{\partial r}{\partial r} + \dot{\theta} \frac{\partial r}{\partial \theta} - r \dot{\theta}^2 \end{aligned} \quad -(6)$$

$$\begin{aligned} \text{and } \frac{Dv_\theta}{Dt} &= \frac{\partial v_\theta}{\partial t} + \left(v_r \frac{\partial v_\theta}{\partial r} + \frac{v_\theta}{r} \frac{\partial v_\theta}{\partial \theta} + \frac{v_\theta v_r}{r} \right) \\ &= \frac{\partial v_\theta}{\partial t} + \left(r \ddot{\theta} + 2 \dot{r} \dot{\theta} + r \dot{\theta} \frac{\partial \theta}{\partial r} + \dot{\theta} \frac{\partial r}{\partial \theta} \right) \end{aligned}$$

Eqs. (6) and (7) can be expressed as the Cartesian

derivative:

$$\frac{D}{Dt} \begin{bmatrix} v_r \\ v_\theta \end{bmatrix} = \frac{d}{dt} \begin{bmatrix} v_r \\ v_\theta \end{bmatrix} + \left(\begin{bmatrix} \frac{\partial v_r}{\partial r} & \frac{1}{r} \frac{\partial v_r}{\partial \theta} \\ \frac{\partial v_\theta}{\partial r} & \frac{1}{r} \frac{\partial v_\theta}{\partial \theta} \end{bmatrix} + \begin{bmatrix} 0 & -\frac{v_\theta}{r} \\ \frac{v_\theta}{r} & 0 \end{bmatrix} \right) \begin{bmatrix} v_r \\ v_\theta \end{bmatrix} \quad -(8)$$

where the quantity inside the brackets on the right hand side is the sp. connection matrix.

Therefore:

$$v_r \frac{dv_r}{dr} + \frac{v_\theta}{r} \frac{dv_r}{d\theta} - \frac{v_\theta^2}{r} = \dot{r} \frac{d\dot{r}}{dr} + \dot{\theta} \frac{d\dot{r}}{d\theta} - r \dot{\theta}^2$$

$$= \begin{bmatrix} \frac{dv_r}{dr} & \frac{1}{r} \frac{dv_r}{d\theta} \\ 0 & 0 \end{bmatrix} \begin{bmatrix} v_r \\ v_\theta \end{bmatrix} + \begin{bmatrix} 0 & -\frac{v_\theta}{r} \\ 0 & 0 \end{bmatrix} \begin{bmatrix} v_r \\ v_\theta \end{bmatrix} \quad (9)$$

and

$$v_r \frac{dv_\theta}{dr} + \frac{v_\theta}{r} \frac{dv_\theta}{d\theta} + \frac{v_\theta v_r}{r} = r \ddot{\theta} + 2 \dot{r} \dot{\theta} + r \dot{\theta} \frac{d\dot{\theta}}{dr} + \dot{\theta}^2 \frac{dr}{d\theta}$$

$$= \begin{bmatrix} 0 & 0 \\ \frac{dv_\theta}{dr} & \frac{1}{r} \frac{dv_\theta}{d\theta} \end{bmatrix} \begin{bmatrix} v_r \\ v_\theta \end{bmatrix} + \begin{bmatrix} 0 & 0 \\ \frac{v_\theta}{r} & 0 \end{bmatrix} \begin{bmatrix} v_r \\ v_\theta \end{bmatrix} \quad (10)$$

Note carefully that the new definition of acceleration, eq. (5), leads to new terms but are absent from the usual development:

$$\underline{a} = \frac{d\underline{v}}{dt} = \frac{d}{dt} (v_r \underline{e}_r) + \frac{d}{dt} (r \dot{\theta} \underline{e}_\theta) \quad (11)$$

$$= (\ddot{r} - r \dot{\theta}^2) \underline{e}_r + (r \ddot{\theta} + 2 \dot{r} \dot{\theta}) \underline{e}_\theta$$

which appear in any good textbook. The acceleration in eq. (11) were inferred by Coriolis 1835. However eq. (5) leads to the new acceleration:

$$\underline{a}_1 = \left(\dot{r} \frac{d\dot{r}}{dr} + \dot{\theta} \frac{d\dot{r}}{d\theta} \right) \underline{e}_r + \left(r \dot{\theta} \frac{d\dot{\theta}}{dr} + \dot{\theta}^2 \frac{dr}{d\theta} \right) \underline{e}_\theta \quad (12)$$

The accelerations (12) are unknown in classical dynamics, they are a fundamental new result of F&E unified field theory. This result for the velocity is considered as a velocity field in fluid dynamics:

$$\underline{v} = \underline{v}(t, r(t), \theta(t)) \quad (13)$$

$$- (14)$$

rather than a classical dynamics. It is a classical development of the plane polar coordinates (e.s. "Vector Analysis Problem Solver"):

$$\frac{dr}{d\theta} = 0 \quad (15)$$

Because r and θ are estimated as the independent variables of the coordinate system (r, θ) . Similarly, $\partial x / \partial t = \partial x / \partial z = \partial / \partial z = 0$ in the Cartesian coordinate system.

However, if r and θ are functions of t , and \underline{v} is a function of $r(t), \theta(t)$ and t , eq. (15) is no longer necessarily true, and the coordinate system is generalized. For example, if an orbit is considered to be the dynamics of the coordinate system itself, an idea of general relativity, then eq. (15) is true for a circular orbit but it is not true in a conic section orbit or precessing ellipse.

In the usual plane polar coordinates eq (15) is not a good coordinate system. This is clear if any good look. Therefore:

$$\frac{d\theta}{dr} = \frac{d}{dr} \left(\frac{d\theta}{dt} \right) = \frac{d\omega}{dr} \quad (16)$$

Let the angular velocity of the coordinate system is $\omega = \dot{\theta} = \frac{d\theta}{dt}$ - (17)

If ω is constant then $\frac{d\dot{\theta}}{dr} = 0$ - (17)

and
$$\underline{a}_1 = \left(\dot{r} \frac{dr}{dr} + \dot{\theta} \frac{dr}{d\theta} \right) \underline{e}_r \quad (18)$$

However if a coordinate system is used in which ω is not a constant, the acceleration:

$$\underline{a}_2 = r \dot{\theta} \frac{d\dot{\theta}}{dr} \underline{e}_\theta \quad (19)$$

is not zero.

Now note that:

$$\frac{dr}{d\theta} = \frac{d}{d\theta} \left(\frac{dr}{dt} \right) = \frac{dr}{d\theta} \quad (20)$$

and
$$\frac{dr}{dr} = \frac{d}{dr} \left(\frac{dr}{dt} \right) = \frac{dr}{dr} \quad (21)$$

In the usual development of the acceleration in plane polar coordinates:

$$\underline{v}_r = \dot{\underline{r}} = \frac{d\underline{r}}{dt} = \frac{d\underline{r}(t)}{dt} \quad - (22)$$

so \underline{v}_r has no functional dependence on r or θ . In consequence:

$$\frac{\partial \underline{v}_r}{\partial \theta} = \frac{\partial \underline{v}_r}{\partial r} = 0 \quad - (23)$$

and

$$\underline{a}_1 = \underline{0} \quad - (24)$$

It follows that:

$$\underline{a} = \frac{D\underline{v}}{Dt} = \frac{\partial \underline{v}}{\partial t} + (\underline{v} \cdot \nabla) \underline{v}$$

$$= \frac{D\underline{v}_r}{Dt} \underline{e}_r + \frac{D\underline{v}_\theta}{Dt} \underline{e}_\theta$$

$$= (\ddot{r} - r\dot{\theta}^2) \underline{e}_r + (r\ddot{\theta} + 2\dot{r}\dot{\theta}) \underline{e}_\theta \quad - (25)$$

P.E.D.

However, eq. (25) is a very limited result that depends on:

$$\underline{v} = \underline{v}(t, r(t), \theta(t)) \rightarrow \underline{v}(t) \quad - (26)$$