

## 237(6): Frenet Analysis of Planar Orbits

In the Frenet analysis the curve  $\underline{r}$  is parameterised as follows:

$$\underline{r} = \underline{r}(s) \quad \text{--- (1)}$$

and the tangent and normal vectors are defined as:

$$\underline{T} = \frac{d\underline{r}}{ds}, \quad \underline{N} = \rho \frac{d\underline{T}}{ds} \quad \text{--- (2)}$$

where  $\rho$  is the radius of curvature. In the plane polar system:

$$\underline{r} = r \cos \theta \underline{i} + r \sin \theta \underline{j} \quad \text{--- (3)}$$

Now define:

$$s = r \quad \text{--- (4)}$$

so

$$\underline{T} = \frac{d\underline{r}}{dr} = \cos \theta \underline{i} + \sin \theta \underline{j} = \underline{e}_r \quad \text{--- (5)}$$

The normal unit vector is defined by:

$$\underline{N} = \rho \frac{d\underline{T}}{dr} = \rho \frac{d\underline{T}}{d\theta} \frac{d\theta}{dr} = \rho \frac{d\theta}{dr} \underline{e}_\theta \quad \text{--- (6)}$$

Since  $\underline{N}$  and  $\underline{e}_\theta$  are unit vectors:

$$\boxed{\rho = \frac{dr}{d\theta}} \quad \text{--- (7)}$$

The curvature of the Frenet system can be defined for any planar orbit by  $dr/d\theta$ . Therefore:

$$\rho = \frac{dr}{d\theta} = \frac{ds}{d\theta} \quad \text{--- (8)}$$

and:

2)

$$\underline{T} = \underline{e}_r, \quad \underline{N} = \underline{e}_\theta. \quad - (9)$$

The velocity is defined by:

$$\begin{aligned} \underline{v} &= v \underline{e}_r + r \dot{\theta} \underline{e}_\theta \\ &= v \underline{T} + r \omega \underline{N} \\ &= v \underline{T} + r \frac{d\theta}{dr} \frac{dr}{dt} \underline{N}. \end{aligned} \quad - (10)$$

$$\boxed{\underline{v} = v \underline{T} + \frac{vr}{\rho} \underline{N}} \quad - (11)$$

The binormal unit vector is defined by:

$$\underline{B} = \underline{T} \times \underline{N} = \underline{e}_r \times \underline{e}_\theta = \underline{k} \quad - (12)$$

The third Frenet formula is:

$$\frac{d\underline{N}}{ds} = \tau \underline{B} - \frac{1}{\rho} \underline{T} \quad - (13)$$

where  $\tau$  is the Frenet torsion. So:

$$\frac{d\underline{e}_\theta}{dr} = \tau \underline{k} - \frac{1}{\rho} \underline{e}_r \quad - (14)$$

$$= \frac{d\underline{e}_\theta}{dt} \frac{dt}{dr}$$

$$= -\frac{\omega}{v} \underline{e}_r$$

It follows that:

$$\rho = \frac{v}{\omega}, \tau = 0 \quad - (15)$$

for all planar orbits. For a circular orbit:

$$\rho = r \quad - (16)$$

otherwise the Frenet curvature is not the radius  $r$ .

The acceleration is:

$$\underline{a} = (\ddot{r} - r\dot{\theta}^2)\underline{e}_r + (r\ddot{\theta} + 2\dot{r}\dot{\theta})\underline{e}_\theta \quad - (17)$$

The tangential and normal components of velocity are defined by:

$$\underline{v} = v_T \underline{T} + v_N \underline{N} \quad - (18)$$

i.e.  $v_T = \frac{dr}{dt}, v_N = r\omega. \quad - (19)$

The tangential acceleration is:

$$\begin{aligned} \underline{a}_T &= \ddot{r}\underline{e}_r + \dot{r}\dot{\theta}\underline{e}_\theta \\ &= \frac{dv}{dt}\underline{T} + \frac{v^2}{\rho}\underline{N} \end{aligned} \quad - (20)$$

The normal acceleration is:

$$\begin{aligned} \underline{a}_N &= (\dot{r}\dot{\theta} + r\ddot{\theta})\underline{e}_\theta - r\dot{\theta}^2\underline{e}_r \quad - (21) \\ &= \frac{v^2}{\rho}\underline{N} - r\omega^2\underline{e}_r + r\ddot{\theta}\underline{e}_\theta \end{aligned}$$



4)

Note that:

$$\omega^2 = \left(\frac{d\theta}{dr}\right)^2 \left(\frac{dr}{dt}\right)^2 = \left(\frac{v}{\rho}\right)^2 \quad - (22)$$

so

$$\boxed{v = \omega \rho} \quad - (23)$$

for any orbit in a plane.

Therefore:

$$\begin{aligned} \frac{d}{dt} \left( \frac{d\theta}{dt} \right) &= \frac{d}{dt} \left( \frac{d\theta}{dr} \frac{dr}{dt} \right) \\ &= \frac{d}{dt} \left( \frac{v}{\rho} \right) \\ &= \frac{1}{\rho} \frac{dv}{dt} + v \frac{d}{dt} \left( \frac{1}{\rho} \right) \\ &= \frac{1}{\rho} \frac{dv}{dt} - \frac{v}{\rho^2} \frac{d\rho}{dt} \end{aligned} \quad - (24)$$

Therefore:

$$\boxed{\underline{a} = \left( \frac{dv}{dt} - r \left( \frac{v}{\rho} \right)^2 \right) \underline{T} + \left( \frac{r}{\rho} \frac{dv}{dt} - \frac{vr}{\rho^2} \frac{d\rho}{dt} + \frac{2v^2}{\rho} \right) \underline{N}} \quad - (25)$$

The vertical acceleration is:

$$\underline{a}_{in} = \frac{dv}{dt} \underline{T} \quad - (26)$$

5) The centrifugal acceleration is:

$$\underline{a_{\text{cent}}} = -r \left( \frac{v}{\rho} \right)^2 \underline{\underline{I}} \quad \text{--- (27)}$$

The Coriolis acceleration is:

$$\underline{a_{\text{Cor}}} = \left( \frac{2v^2}{\rho} + \frac{r}{\rho} \frac{dv}{dt} + vr \frac{d}{dt} \left( \frac{1}{\rho} \right) \right) \underline{\underline{N}} \quad \text{--- (28)}$$

The Coriolis acceleration vanishes in all planar orbits.

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